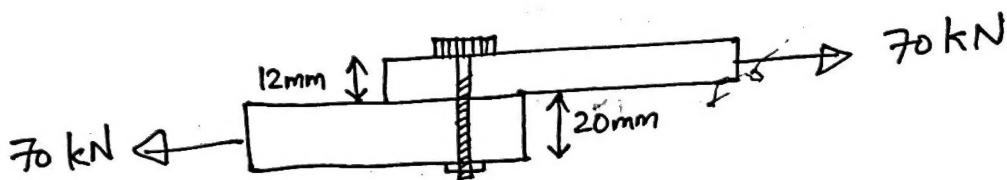


Q1

Design a bolted connection between 2 plates of thickness 12mm & 20mm each, subjected to a load 70 kN. Use M16 bolts of grade 4.6, and Fe 410 grade plates.

Ans:



Design of bolts:

i) Design shear capacity of bolt

(Pg 75 - IS 800 Cl. 10.3.3)

$$V_{dsb} = \frac{f_{ub} (n_n A_{nb} + n_s A_{sb})}{\sqrt{3} \gamma_{mb}}$$

where $f_{ub} = 400 \text{ N/mm}^2$ (\because 4.6 grade bolts)

$\gamma_{mb} = 1.25$ (Pg 30 - Tables of IS 800)

$$n_n = 1$$

$$n_s = 0$$

$$A_{nb} = 0.78 \frac{\pi}{4} \times 16^2 = 157 \text{ mm}^2$$

$$A_{sb} = 0$$

$$\Rightarrow V_{dsb} = \frac{400 (1 \times 157 + 0)}{\sqrt{3} \times 1.25} = 29006 \text{ N}$$

$$= \underline{\underline{29.01 \text{ kN}}}$$

(ii) Design bearing capacity of bolt (Pg 75 - IS800)
(Cl. 10.3.4)

$$\sqrt{dpb} = \frac{2.5 k_b d t f_u}{\gamma_{mb}}$$

where $d = 16 \text{ mm}$

$t = 12 \text{ mm}$ (thinner plate)

$$f_u = 410 \text{ N/mm}^2$$

$$k_b = \text{smaller of } \left\{ \begin{array}{l} e/3d_0 = \frac{27}{3 \times 18} = 0.50 \\ p/3d_0 - 0.25 = \frac{40}{3 \times 18} - 0.25 = 0.49 \\ f_{ub}/f_u = \frac{400}{410} = 0.98 \end{array} \right.$$

Assume $d_0 = 16 + 2 = 18 \text{ mm}$ (Refer Table 19 - page 73 of IS800)

$$e = 1.5 d_0 = 1.5 \times 18 = 27 \text{ mm}$$

(refer Pg 74 - Cl. 10.2.4.2 - machine cut)

$$P = 2.5 d = 2.5 \times 16 = 40 \text{ mm}$$

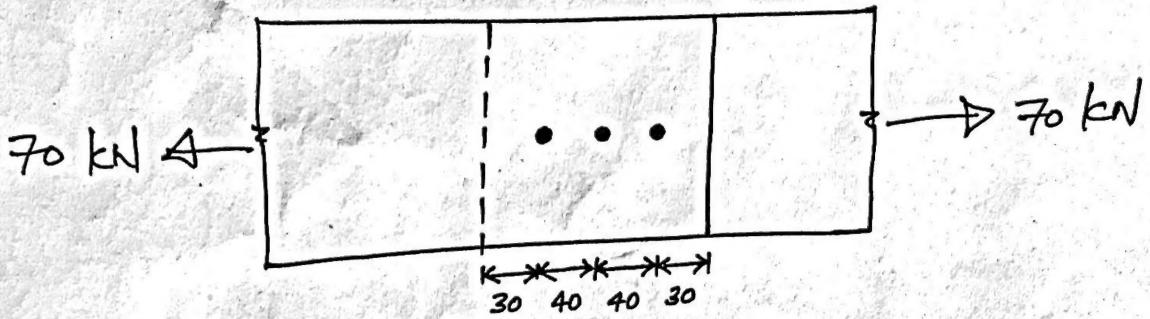
(refer Pg 73 - Cl. 10.2.2 - pitch)

$$\Rightarrow \sqrt{dpb} = \frac{2.5 \times 0.49 \times 16 \times 12 \times 410}{1.25}$$

$$= 77146 \text{ N} = \underline{\underline{77.15 \text{ kN}}}$$

\therefore Bolt value = smaller of bolt capacities
= 29.01 kN

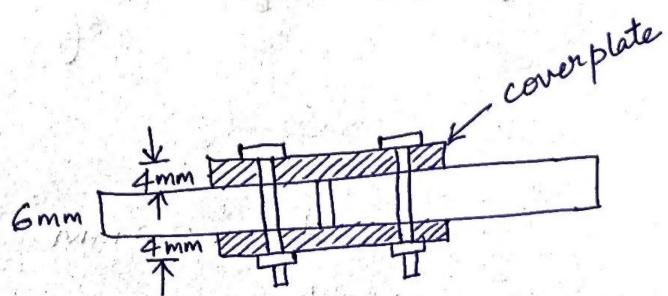
$$\text{No. of bolts required} = \frac{70}{29.01} \approx \underline{\underline{3 \text{ nos}}}$$



Q2

Q. A ~~single-bolted~~ double cover butt joint is used to connect two plates 6 mm thick. Assuming 4.6 grade M20 bolts and 4 mm thick cover plates. Plates are of grade Fe410. Design the joint, if requires to transfer a force of 100 kN.

Ans:-



Shear capacity of bolt

$$V_{dsb} = \frac{f_{ub}}{\sqrt{3}} \left(n_n A_{nb} + n_s A_{sb} \right)$$

where $f_{ub} = 400 \text{ N/mm}^2$ (for 4.6 grade bolts)

$$\gamma_{mb} = 1.25 \quad (\text{Table 5 - Pg 30})$$

$n_n = 1$ } there are two shear planes
 $n_s = 1$ } each passing through
 thread & shank

$$A_{nb} = 0.78 \frac{\pi}{4} \times 20^2 = 245 \text{ mm}^2$$

$$A_{sb} = \frac{\pi}{4} \times 20^2 = 314 \text{ mm}^2$$

$$\Rightarrow V_{dsb} = \frac{400}{\sqrt{3}} \left[(1 \times 314) + (1 \times 245) \right] \div 1.25$$

$$= 103.28 \text{ kN}$$

Bearing capacity of bolt

$$V_{dpb} = \frac{2.5 k_b d t f_u}{\gamma_{mb}}$$

where ~~γ_{mb}~~ =

~~γ_{mb}~~ =

where $k_b = \text{smaller of } \begin{cases} e/3d_0 \\ P/3d_0 - 0.25 \\ f_{ub}/f_u \\ 1 \end{cases}$

$$d = 20 \text{ mm}$$

$$d_0 = 20 + 2 = 22 \text{ mm} \quad (\text{Pg 73 - Table 19})$$

$$e = 1.5 d_0 = 1.5 \times 22 = 33 \text{ mm} \quad (\text{Pg 74 - Cl. 10.2.4.2})$$

$$\phi = 2.5 d = 2.5 \times 20 = 50 \text{ mm} \quad (\text{Pg 73 - Cl. 10.2.2})$$

$$f_{ub} = 400 \text{ N/mm}^2$$

$$f_u = 410 \text{ N/mm}^2$$

$$\Rightarrow k_b = \text{smaller of } \begin{cases} \frac{33}{3 \times 22} = 0.50 \\ \frac{50}{3 \times 22} - 0.25 = 0.51 \\ \frac{400}{410} = 0.98 \\ 1 \end{cases} \} = 0.50$$

$$t = \text{smaller of } \begin{cases} 6 \text{ mm} \\ 4 + 4 = 8 \text{ mm} \end{cases} \} = 6 \text{ mm}$$

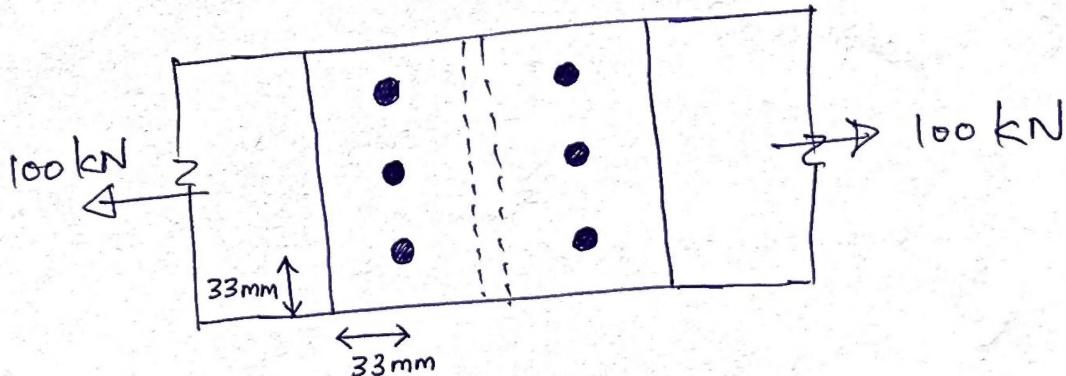
$$V_{dpb} = \frac{2.5 \times 0.5 \times 20 \times 6 \times 400}{1.25}$$

smaller of f_u & f_u

$$= \underline{\underline{48 \text{ kN}}}$$

∴ Strength of bolt
or
Bolt value = Smaller { V_{dsb}
 V_{dpb} }
= 48 \text{ kN}

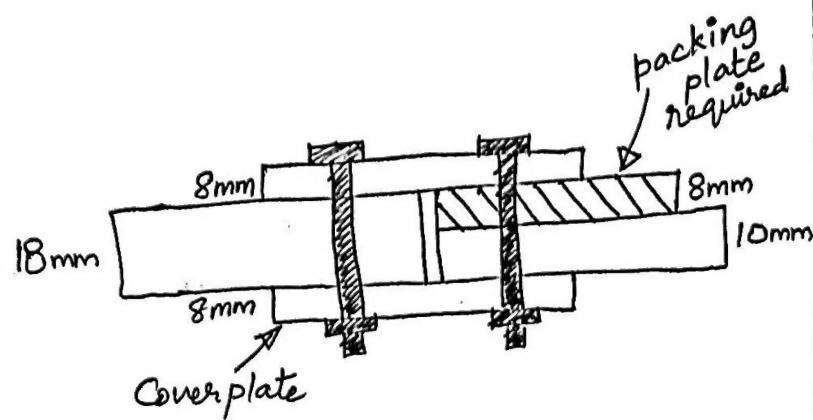
∴ No. of bolts required on
each side of the double-cover
butt joint = $\frac{100}{48} \approx \underline{\underline{3 \text{ nos}}}$



(Q:)

Determine the design shear capacity of bolt for a joint comprising 10mm & 18mm thick plates connected by two coverplates of 8mm thick. Use M20 bolts of 4.6 grade.

Ans:



Shear capacity of bolt

$$V_{dsb} = \frac{f_{ub}}{\sqrt{3}} \cdot \frac{(n_n A_{ub} + n_s A_{sb})}{\gamma_{mb}}$$

where $f_{ub} = 400 \text{ N/mm}^2$

$$\gamma_{mb} = 1.25$$

$n_n = 1 \left. \right\}$ two shearplanes, each passing through shank & thread
 $n_s = 1 \left. \right\}$

$$A_{ub} = 0.78 \pi/4 \times 20^2 = 245 \text{ mm}^2$$

$$A_{sb} = \pi/4 \times 20^2 = 314 \text{ mm}^2$$

$$\Rightarrow V_{dsb} = \frac{400 [(1 \times 245) + (1 \times 314)]}{\sqrt{3} \cdot 1.25}$$

$$= \underline{\underline{103.28 \text{ kN}}}$$

Since a packing plate of thickness exceeding 6mm is used, reduction factor (β_{pk}) is required to be multiplied.

$$\begin{aligned}\beta_{pk} &= 1 - 0.0125 t_{pkg} \\ &= 1 - (0.0125 \times 8) \\ &= \underline{\underline{0.90}}\end{aligned}$$

Design shear capacity of bolt

$$= V_{dsb} \times \beta_{pk}$$

$$= 103.28 \times 0.90$$

$$= \underline{\underline{92.95 \text{ kN}}}$$